On the Impulsive Nature of Interchannel Interference in Digital Communication Systems

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Courtesy of John B Lancaster



- Transmit a tone modulated by a 'smooth'-looking message
- Observe instantaneous power in an out-of-band receiver
 - impulsive pulse train

Signal traces





- Some peaks originate at zero modulation amplitude
 - at onsets and ends of modulating pulses



 Others originate at 'smoothest', most linear parts of modulating pulses

Elemental model

Setup

- Transmitter
 - linear combination of terms $x(t) = A_T(\bar{t}) e^{i\omega_c t}$
 - $A_T(\bar{t})$ is complex-valued modulation, and $\bar{t} = \frac{2\pi}{T} t$
- Receiver
 - quadrature receiver at $f_c + \Delta f$ with baseband impulse response $w(t) = \frac{2\pi}{T} h(\bar{t})$
- Signal in the receiver

$$egin{aligned} &I(t,\Delta f)+\mathrm{i}Q(t,\Delta f)=\ &\int_{-\infty}^{\infty}\!\!\!\mathrm{d} au\;\mathcal{A}_{T}(ar{ au})\,w(t- au)\,\mathrm{e}^{\mathrm{i}\Delta\omega au} \end{aligned}$$

• windowed Fourier transform of x(t)

Elemental model

Analysis

Use consecutive integration by parts:

$$\begin{split} I(t,\Delta f) + \mathrm{i} Q(t,\Delta f) = \\ \frac{\mathrm{i}^n}{(T\,\Delta f)^n} \int_{-\infty}^{\infty} \mathrm{d}\bar{\tau} \, \mathrm{e}^{\mathrm{i}\,(T\,\Delta f)\,\bar{\tau}} \times \frac{\mathrm{d}^n}{\mathrm{d}\bar{\tau}^n} \left[A_T(\bar{\tau}) \, h\left(\bar{t} - \bar{\tau}\right) \right] \end{split}$$

- ► Note that A_T(t̄) is convolution of discrete signal and causal impulse response
 - differentiate until 'singular' component(s) appear

Then, for example:

$$P_{x}(t,\Delta f) = \frac{1}{(T\Delta f)^{2n}} \sum_{i} |\alpha_{i}|^{2} h^{2} (\overline{t} - \overline{t}_{i})$$

- for sufficiently large T and Δf
- impulsive pulse train
- $|\alpha_i|$ is magnitude of discontinuity of $A_T^{(n-1)}(\bar{t})$ at \bar{t}_i



Raised cosine pulse shaping: Simulated idealized example



Raised cosine pulse shaping: Simulated spectrogram



Interference pattern with non-idealities



It follows:

- Impulsive nature of out-of-band interference results from causal nature of communications
- Effect can always be measured, may or may not be negligible
 - made stronger and more complicated by non-idealities in transmitter
 - enhanced by external EMI distortions from digital circuitry
- May motivate usage of nonlinear filtering techniques in the receiver
 - non-Gaussian interference makes nonlinear techniques effective

Appendix I



Appendix II

Discontinuities in Continuous Phase Modulation

Transmitted signal:

$$x(t) = A_{T}(\overline{t}) e^{\mathrm{i}\omega_{c}t} = \left[A_{0} e^{\mathrm{i}(T \Delta f_{c}) \int_{-\infty}^{\overline{t}} \mathrm{d}\tau \, \mathbf{a}_{T}(\tau)}\right] e^{\mathrm{i}\omega_{c}t},$$

where Δf_{c} is the frequency deviation

• Derivative of
$$A_T(\overline{t})$$
:

$$A_T'(\bar{t}) = \mathrm{i}(T \Delta f_\mathrm{c}) A_T(\bar{t}) a_T(\bar{t})$$

• Then, if $a_T^{(n-2)}(\bar{t})$ contains discontinuities, so does $A_T^{(n-1)}(\bar{t})$

Appendix III

Impulsive noise and SPART filters: Linear vs nonlinear



Appendix IV

EMI from WiFi/Bluetooth in GPS: Bench setup



Appendix V

EMI from WiFi/Bluetooth in GPS: Scope traces



Appendix VI

Peakedness (impulsiveness) of EMI: EMI from WiFi in GPS



Appendix VII

Mitigating impulsive EMI in GPS: Test at GPS company

